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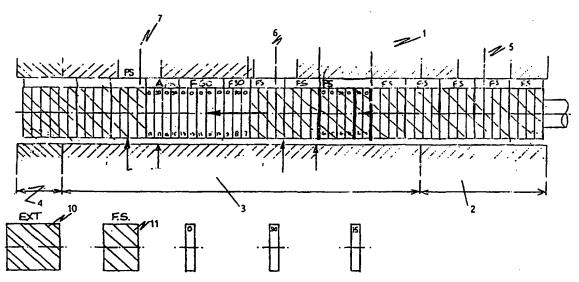
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(57) Abstract

A method of manufacturing a biodegradable plastics material comprising the following steps: (a) mixing a stabiliser with a partially hydrolysed, water-soluble polyvinyl alcohol (PVA) co-polymer; (b) adding a plasticiser to the mixture of stabiliser and PVA; and (c) mixing the PVA, plasticiser and stabiliser at a temperature in the range of between 106 to 140 °C whereby the resultant material can readily be worked by known processes and is suitable for the manufacture of water soluble and biodegradable articles, optionally, after the mixing stage, the method includes the steps of compounding and pelletising the resultant product to produce a useable, commercial pellet wherein the compounding is carried out at a temperature in the range 195 - 225 °C. The method includes processing the plastics material further by blow moulding, cast extrusion, injection moulding or any other suitable type of process currently in use. The invention also discloses an article produced by the above method.

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BIODEGRADABLE PLASTIC MATERIAL AND A METHOD FOR ITS MANUFACTURE

The present invention relates to a biodegradable plastics material and to a method for its manufacture. In particular, the invention relates to a biodegradable plastics material comprising a polyvinylacetate/polyvinylalcohol copolymer.

Commercially available biodegradable plastics do not fully degrade in the environment and retain a high degree of toxicity when partially degraded. Furthermore, such materials are expensive and generally only used for niche markets.

The use of polyvinylacetate/polyvinylalcohol (PVA) copolymers for the

15 manufacture of biodegradable plastics materials is described in

W092/01556. By layering or surrounding PVA which is water soluble at

20°C with a thin layer of a PVA which is water insoluble at 20°C, an

article which is protected from dissolution by water until its

waterproofing, insoluble layer is breached may be manufactured. The

20 PVA's are co-extruded as a laminate or may be moulded, with or without an
intervening filler layer. Water soluble PVA dissolves readily in water—

and is broken down in the environment within a relatively short time to
carbon dioxide and water.

25 German Patent No. 1127085 discloses that in order to process PVA plastics material on standard processing apparatus such as profile extruding machines, blown film extruders or injection moulding machines, undesirable thermal decomposition of the products occurs at temperatures above 150°C amd must be prevented by external plasticising of granular plastics material. The plastics material is plasticized by mixing with a suitable plasticizer for 15-30 mins. at a temperature of up to 1:0°C. This plasticized PVA can be injection moulded and extruded under the following conditions: heating the material to a temperature in the range 145-190°C and at an injection pressure of 100-130 bar.

While PVA is known as a biodegradable material, its use in the

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manufacture of plastic articles has up to now been limited as it is technically difficult to work with this material and to produce an acceptable product, therefore it is costly and commercially unsuccessful.

- The present invention seeks to provide an improved plastics material comprising a PVA copolymer which can readily be worked by known processes such as blow moulding, injection moulding, cast extrusion, etc. and which is suitable for the manufacture of biodegradable articles.
- The term PVA as used herein refers to a polyvinylacetate polymer which has been partially hydrolysed to convert a proportion of the acetate groups to the corresponding alcohol. Therefore, the term refers to a polyvinylacetate/ polyvinylalcohol copolymer. The solubility of the PVA is dependent, inter alia, on the degree to which the PVA is hydrolysed.
- "Cold soluble" PVA denotes a copolymer which is generally referred to as "partially hydrolyzed" polyvinylacetate. Typically, the partially hydrolyzed copolymer comprises 70 to 85 wt % of the alcohol, with the remainder comprising residual acetate, and this material is soluble in "cold" water. It is generally readily soluble in water at 20°C. Further
- hydrolysis of the PVA to levels at which the alcohol comprises about 96 mol % or greater (usually referred to as "fully hydrolyzed" polyvinylalcohol, results in a marked decrease in solubility. While the fully hydrolysed polymer is usually thought of as insoluble, it is in fact soluble in water at a temperature of about 50°C or greater. Such
- 25 material is referred to herein as "hot soluble" PVA. Both hot and cold soluble PVA's, once dissolved, are fully biodegradable in nature to $\rm CO_2$ and $\rm H_2O$. The undegraded copolymers and their partially degraded derivatives are non-toxic.
- 30 The present invention provides a method of manufacturing a biodegradable plastics material comprising mixing partially hydrolysed, water soluble polyvinyl alcohol (PVA) co-polymer with a plasticiser and stabiliser at a temperature in the range of between 106 to 140°C, whereby the resultant material can readily be worked by known processes and is suitable for the manufacture of water soluble and biodegradable articles.

The method may comprise the following steps:

- a. mixing the stabiliser with the PVA; and
 - b. adding the plasticiser to the mixture of stabiliser and PVA and mixing at a temperature between 106 to 140°C.
- After the mixing stage, the method may include the steps of compounding and pelletising the resultant product to produce a useable, commercial pellet wherein the compounding is carried out at a temperature in the range 195 225°C.
- The method may include processing the plastics material further by blow moulding, cast extrusion, injection moulding or any other suitable type of process currently in use.
- The mixing stage may include mixing PVA and stabiliser are mixed in $a^{\prime\prime}$ forced action blender.

The stabiliser may be included in an amount in the range of 4 to 6% w/w (weight of stearamide to weight of PVA) and the plasticiser is included in an amount in the range of 3 to 15% w/w (weight of plasticiser to weight of PVA).

The stabiliser may stearamide or a stearate and the plasticiser may comprise glycerol or glycerine solution or soya bean oil.

The mixing stage may be carried out at a temperature in the range of 123 to 129°C.

The method may include the step of applying a waterproofing agent to at least a portion of the surface of the plastics material so that at least a portion of the material is rendered resistant to water to prevent premature dissolution of the product on contact with water.

The waterproofing agent may be phenoxy resin.

5 The invention also provides a fully or substantially fully biodegradable article produced by the method of the invention.

According to the invention, the addition of a stabiliser to the PVA feedstock during compounding of the plastics material results in a product which can readily be worked into a product by any of the commonly used methods. The PVA feedstock may be cold or hot soluble, partially hydrolysed PVA which is 70-85 wt % polyvinyl alcohol. A broad range of polymer molecular weights are suitable for use, depending on the desired characteristics of the final product. Generally, molecular weights in the range of 20,000 d to 90,000 d are usable. Plastics made from PVA's falling into the lower part of this range will be softer and pliable, and will be suitable for making relatively flimsy films. Selection of PVA's from the upper end of the range will allow much harder plastics to be made, for example for making articles such as bottles, moulds, bowls, The preferred molecular weight range is from about 50,000 d to about 60,000 d, degree of hydrolysis 76.7-79.3 mol%. PVA's in this range, when compounded as described herein, may readily be extruded to give good quality product.

The most preferred stabiliser for use in the manufacture of the plastics material is stearamide (octadecanamide), which is a fully biodegradable substance. Alternatively stearates such as zinc stearate can also be used. Stearamide is added in the range of between about 4 to 6 wt %, with 5 wt % being preferred.

A plasticiser is also added and preferably this will also be a biodegradable substance. Typically, the plasticiser will be glycerol or glycerine and will be present in the range of between about 3 to 15 wt %, preferably 5 to 10 wt % and optimally about 5 wt %. The stearamide and glycerol in combination provide an excellent stabilising/plasticising effect in the plastics material. The rigidity of the plastics product

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can be controlled by varying the amount of glycerol and stearamide added, the product becoming softer and more pliable as the weight % of stearamide and/or glycerol is increased.

5 Other additives, well known in the art, may also be used in compounding the plastics material according to the invention. Such additives may include colouring compounds and fillers.

The plastics material may be compounded by any suitable means known in the art. Most preferably, the PVA feedstock in the form of powder or granules is mixed with the stearamide, glycerol and optional other ingredients in a forced action blender. However achieved, the mixing will be done at an elevated temperature of between 106 to 140°C, preferably between 123°C and 129°C when film will be blown subsequently, and optimally about 125°C. After mixing, the plastics material may be pelleted or otherwise prepared, ready for forming into a desired article by extrusion, moulding or otherwise.

The article prepared in this way will be fully or almost fully

20 biodegradable. When it is to be discarded to waste, it need only be brought into contact with water, either cold or hot, depending on the PVA feedstock chosen, to cause it to dissolve. The dissolved PVA will then be fully biodegradable within about 28 days to CO₂ and H₂O. Likewise, the biodegradable additives in the plastics material will degrade. The

25 PVA in itself is non-toxic and therefore poses no environmental hazard during the time during which it is being biodegraded.

Clearly, the plastics material described above is suitable only for the manufacture of articles which do not, or are unlikely to, come into contact with water during their normal usable life. According to another aspect of the invention, a PVA plastics articles which is at least partially waterproof, water resistant or hydrophobic is provided. Water resistance will be required in any article which during its normal storage or use, is in contact with an aqueous environment or a humid environment. Those surfaces of the article which are exposed to the

aqueous or humid environment need to be protected from that environment until such time as the article is to be discarded to waste. Examples of such articles include, without limitation, plastic bags, sachets, sacks, wrappers, packaging and the like, films, containers including bottles, jars, beakers, pots and the like and liners including sanitary products such as napkins, nappy liners and the like. Many other applications will suggest themselves to the skilled person. In some cases, all surfaces of the article will require to be rendered waterproof while in other cases, only a portion of the article need be so treated. However waterproofed, the article will easily be disposed of after use. In the case where only a portion of the article has been made water resistant, contacting the untreated portion of the article with water will cause the article as a whole to dissolve. Where all exposed surfaces of the article have been waterproofed, then for disposal, the article need only be broken to expose its interior to the aqueous solvent and thereafter, dissolution of the entire article will occur.

The waterproofing may be achieved in any suitable way or combination of ways, as will now be described.

- (1) Polymer Crosslinking. A thin layer of the surface of the article may be made water resistant by crosslinking the copolymer. One way of achieving this is to add an ultra-violet sensitiser to the PVA during compounding, for example sodium benzoate, benzamide, benzoic acid or tetrazolium salts. After forming an article from the plastics material, the article is subjected to ultra-violet irradiation, during which the sensitiser promotes crosslinking of the polymer chains at the irradiated surface, rendering the crosslinked polymers insoluble, with the effect that a thin layer of the PVA at the surface of the article becomes water resistant. Optionally, a migrating agent may be added to assist the movement of the sensitiser to the surface. Alternatively, the sensitiser may be applied to the surface of the article after manufacture and prior
- 35 (2) Silanisation. The article or a surface thereof may be coated with

to irradiation.

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- 7 -

silane. The silane may be in liquid or gaseous form. The article may be bathed in a silane, or the silane may be applied to the article by dipping, spraying or painting. This is valid for light water resistance.

(3) Treatment with other waterproofing compound. A waterproofing compound may be added to the PVA feedstock during compounding of the plastics material. This compound may be a hydrophobic substance. A migrating agent may be added to assist movement of the waterproofing compound to the surface of the article formed from the plastics material. The waterproofing agent may itself be a migrating agent. As an

alternative to compounding the waterproofing agent into the plastics, it may be applied to the finished article by dipping, spraying or painting. One suitable waterproofing agent is phenoxy resin. Polyvinylacetate or other suitable, non-toxic polymer may be used as a surface coat on the PVA article. To assist adhesion of the waterproofing agent to the surface of the article, it may be treated for example by electrical treatment prior to coating to condition the surface so as to render it more able to accept and retain the waterproofing coating.

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In some cases, it will be appropriate to manufacture the article from hot soluble PVA. Provided that the article does not encounter water at a temperature in excess of about 45°C during its normal use, such a product need not be surface water-proofed. After use, placing the object in water heated to at least 50°C will promote its dissolution for disposal. An article prepared in this way will be fully or almost fully biodegradable.

The invention will now be described more particularly with reference to the following non-restrictive examples and to Figure 1 of the drawings in 30 which is shown an embodiment of the screw design used in the apparatus at the compounding stage of the process of the present invention.

Example 1

35

Mixing Stage

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A Prism lab 6 high speed mixer was used (Henschel 50kg mixer also used).

Ingredients

5 5kg PVA (degree of hydrolysis of 76.7 to 79.3 mol%)
0.25 kg stearamide (5% w/w of stearamide to weight of PVA)
0.25 kg of glycerol (5% w/w of glycerol to weight of PVA)

A high speed forced action blender was used. The PVA and stearamide were added to the mixer and mixed for 1 minute. The glycerol was added slowly over a period of 30 seconds, with the mixer rotating at approximately 500 rpm. As a result of the agitation, the mix became frothy ("fluffed up") and the mixer was stopped to push mixed material from the inside of the mixer. After 2-5 minutes, the mix had settled down and the mixer was turned up to full speed, from 1,500 rpm to 3,000 rpm. As a result of the kinetic energy generated by the agitation of the mix, the temperature increased to 123° and went to 125° in 8 to 20 minutes depending on the type of mixer used.

20 The temperature is a critical parameter to achieving high quality product.

A vacuum was created at the top of the mixer to draw off any moisture vapour which had formed at the top of the mixer and which would otherwise condense back into the mix.

The mix was allowed to cool to $60-70^{\circ}$ C so that it was sufficiently cool to allow it to be bagged. The mix can be allowed to cool by itself or optionally a heating/cooling jacket can be included on the mixer vessel.

Alternatively mix can be transferred to another vessel to cool. The mixture was stirred occasionally to help cooling and break up any lumps which had formed. The product is in granular form and is bagged in air-tight bags.

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- 9 -

Compounding/pelleting stage

A Prism TSE 16TC twin screw extruder with 4 1/2mm die was used for the compounding stage.

5

The temperature range was 200°C - 218°C measured from the feed end of the screw to the die end.

The extruder is vented along the screw to allow moisture vapour to exit

10 the screw because otherwise bubbles occur in the strands. The product
emerges from the extruder in the form of a strand which has elastic
properties. The strands must be dried in air using air knives, for
instance, and not in water. After cooling, the strands were cut into
pellets using a Prism LPT 16 laboratory pelletiser. The pellets were

15 then bagged in an air tight fashion.

The screw design of the twin screw extruder is shown in Figure 1. A single screw apparatus could also be used for compounding.

20 Referring to Figure 1, the screw is indicated generally by reference numeral 1 and includes three zones, namely a feed zone 2, a work zone 3 and a die zone 4.

The feed enters the screw through a feed port 5. Two other ports 6, 7

25 are included along the length of the screw, to allow for addition of material if required, (6) and for venting (7) respectively. A heating band and a temperature probe respectively are included at two locations along the length of the screw.

30 The configuration of the screw includes several elements namely an extrusion screw indicated by the letters EXT (length = 1.5 times the diameter) and feedscrew elements indicated by the letters FS (length equal to its diameter). The screw also includes mixing elements (length = diameter divided by 4) which may be 0° offset, 90° offset or 15° offset. The mixing elements may be forwarding (F), reversing (R) or

- 10 -

alternating (A).

Blowing film

A Betol 0250 film tower machine was used.

The temperature profile along the screw extruder is as follows:

Feed zone of barrel $195-210^{\circ}$ C

Work zone of barrel $200-218^{\circ}$ C

Die zone $200-218^{\circ}$ C

Screens of 200/inch² gauge size are used to soften the memory of the PVA

and reduce the risk of any possible extraneous matter and gels. Further

screens are also provided of 40/inch²,60/inch², 80/inch², 100/inch² and

120/inch² secured to the 200/inch² screen to give it strength.

Screens are located between the end of the screw and the die.

20 Spraying the waterproofing agent, phenoxy resin, onto the film

Mixing (before spraying)

25

100g phenoxy resin was mixed with 500mls Methyl Ethyl Ketone (MEK)

initially to 20% w/w solids. This is mixed in a high speed mixer or is left to stand at a temperature of a minimum of 28°C for 3-5 days with periodic shaking to achieve a solution. When the phenoxy resin was in solution, a mixture comprising 500 mls of MEK and 12mls water was added to the solution. Thus the phenoxy resin was then in solution at a concentration of approximately 10% w/w.

A 10% w/w solution of phenoxy resin was used for spraying a film of thickness 40 /um. Alternatively 5% or 2.5% solution of phenoxy in MEK with water added was also be used depending on the thickness of the film to be sprayed. Lower concentrations of phenoxy resin in MEK with water

- 11 -

may also be used.

Spraying

Spraying was carried out in dry conditions and preferably at a minimum temperature of 21°C. A Campbell Hausfeld Professional Turbo Spray (high volume/low pressure finishing system HV2,000) was used for spraying but conventional sprayers may also by used. The humidity of the atmosphere in which spraying is being conducted is a critical parameter. The film was sprayed so as to achieve good cover but without overspraying. Thin film below 40 µm needs stretching so that no folds occur during spraying and must be held flat. Heavier plastics must also be held flat. Alternatively, heavier plastics (60 µm+) can be dipped or use sponge or roller to apply.

15

Example 2

Mixing stage

20 <u>Ingredients</u>

5 kg PVA (degree of Hydrolysis of 76.7 to 79.3 mol %)
0.5 kg glycerol (10% w/w) glycerol
0.25 kg (5% w/w) stearamide

25

The procedure is the same as in the mixing stage described in Example 1.

Compounding/pelletising stage

30 The temperature profile along the screw extruder was as follows:

Feed zone of barrel 200°C Work zone of barrel 205°C Die zone 210°C

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Rpm 260

Output 2.5kg/hr approximately

Example 3

5

Mixing stage

5 kgs PVA

0.75 kg glycerol (15%w/w) glycerol

10 0.25 kg (5%w/w) stearamide

Compounding/pelletising stage

Feed zone of barrel 200°C

Work zone of barrel 215°C

15 Die zone 216°C

Rpm 260⁰

Output 2.5kg/hr approximately.

20 Further Examples of parameters at the compounding and blowing stages

A Prism TSE 16TC apparatus was used for compounding with a blow line attachment for blowing film.

25 The temperature of the various zones is given in 0 C in the following examples.

Example 4

Film

30	Blowing	Die	Work	Feed
	Zone	<u>Zone</u>	Zone	Zone
	215	209	207	200

35 Good quality film was produced.

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	Example 5				
		Film			
5		Blowing	Die	Work	Feed
		Zone	Zone	Zone	Zone
		215	209	209	197
		•		2	
10	Pressure		(4000-4500 k		
		(pressure	at exit end	of screw)	
	Feed	0.5			
	rpm	303			
15	Example 6				
		Film			
		Blowing	Die	Work	Feed
		Zone	Zone	Zone	<u>Zone</u>
		54.5			
20	•	215	212	209	199
	Pressure	40-45 bar	(4000-4500 ki	N/m ²)	
	Torque	7.8 -8.0 N		,,,,,	
	Rpm	301			
2.5					
25	Example 7				
		Film			
		Blowing	Die	Work	Feed
		Zone	Zone	Zone	Zone
30					
		195	202	191	183
	Pressure	60 bar (60	00 kn/m ²)		
	Torque	8.0-8.4 NM			

These parameters resulted in poor quality film.

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Example 8

Film

 Blowing
 Die
 Work
 Feed

 Zone
 Zone
 Zone

 188
 201
 188
 182

Pressure

75 bar (7500 kN/M^2)

10 Torque

5

8.6 NM

These parameters also resulted in production of poor quality film.

Example 9

15 Film

Blowing	Die	Work	Feed
Zone	Zone	<u>Zone</u>	<u>Zone</u>
182	202	189	182

20

These parameters resulted in the production of poor quality film.

Example 10

Film

 Zone
 Zone
 Zone
 Zone
 Zone

 192
 197
 181
 176

30 These parameters also resulted in production of poor quality film.

- 15 -

177

171

Example 11

Film

192

Blowing Die Work Feed

Zone Zone Zone Zone

It was not possible to produce film at these temperatures.

191

10 Example 12

5

15

Film

Blowing Die Work Feed

Zone Zone Zone Zone

213 212 208 200

Pressure 45 bar (4500 kN/m^2)

Rpm 301

20
Good quality film was produced.

Example 13

Film

25 Blowing Die Work Feed Zone Zone Zone 214 211 207 200

30 Pressure 40-45 bar $(4000-4500 \text{ kN/M}^2)$ Torque 8-8.5 NMFeed 0.35

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Ex	amp	ole	14

	Film			
	Blowing	Die	Work	Feed
5	Zone	Zone	<u>Zone</u>	<u>Zone</u>
	219	214	215	202

Good quality film was produced.

10 Example 15

	Film			
	Blowing	Die	Work	Feed
	Zone	<u>Zone</u>	<u>Zone</u>	Zone
15	222	218	216	203

Good quality film was produced.

Example 16

Film			
Blowing	Die	Work	Feed
Zone	<u>Zone</u>	<u>Zone</u>	<u>Zone</u>
225	220	219	204
	Blowing Zone	Blowing Die Zone Zone	Blowing Die Work Zone Zone Zone

These parameters resulted in borderline quality.

Example 17

	Film				
30	 - Blowing	Die	Work	Feed	-
	Zone	Zone	Zone	<u>Zone</u>	
	229	221	221	204	

35 Poor quality film was produced.

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	Example 18				
		Film			
		Blowing	Die	Work	Feed
5		Zone	Zone	Zone	Zone
		228	223	224	205
	Poor quality	film was pr	oduced.		
10					
	Example 19			•	
	•	Film			
		Blowing	Die	Work	Feed
		Zone	<u>Zone</u>	<u>Zone</u>	<u>Zone</u>
15					
		228	226	227	206
		611			
	Poor quality	riim was pr	oaucea.		
20	Example 20				
20	Example 20	Film			
20	Example 20	Film Blowing	Die	Work	Feed
20	Example 20		Die <u>Zone</u>	Work Zone	Feed Zone
20	Example 20	Blowing		Work Zone	Feed <u>Zone</u>
20	Example 20	Blowing			
	Example 20	Blowing Zone	<u>Zone</u>	<u>Zone</u>	Zone
	Example 20 Poor quality	Blowing Zone 228	<u>Zone</u> 229	<u>Zone</u>	Zone
	Poor quality	Blowing Zone 228	<u>Zone</u> 229	<u>Zone</u>	Zone
	,	Blowing Zone 228	<u>Zone</u> 229	<u>Zone</u>	Zone
	Poor quality	Blowing Zone 228 film was pro	<u>Zone</u> 229	<u>Zone</u>	Zone
25	Poor quality	Blowing Zone 228 Film was pro	<u>Zone</u> 229	<u>Zone</u>	Zone
25	Poor quality	Blowing Zone 228 film was pro	Zone 229 oduced.	<u>Zone</u> 231	<u>Zone</u> 206
25	Poor quality	Blowing Zone 228 film was pro Film Blowing Zone	Zone 229 oduced. Die Zone	Zone 231 Work Zone	Zone 206 Feed Zone
25	Poor quality	Blowing Zone 228 film was pro Film Blowing	Zone 229 oduced.	Zone 231 Work	Zone 206 Feed

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Poor quality film was produced.

Example 22

Film

 Blowing
 Die
 Work
 Feed

 Zone
 Zone
 Zone
 Zone

 238
 230
 231
 206

10 It was not possible to blow film from the material exiting the screw extruder at these temperatures.

Example 23

Film

Blowing Die Work Feed

Zone Zone Zone Zone Zone

213 210 207 201

20 Good quality film was produced.

Pressure

35-40 bar $(3500-4000 \text{ kN/m}^2)$

Torque

7.6-8.0 NM

25 Rpm

302

Example 24

Film

Blowing Die Work Feed

Zone Zone Zone Zone Zone

211

208

201

Good quality film was produced.

212

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Example 25

	<u> </u>				
		Film			
		Blowing	Die	Work	Feed
		Zone	Zone	Zone	Zone
5					
		213	210	204	194
	Good quality	film was pr	oduced.		
10	D	40.45.1		2 .	
10	Pressure		(4000-4500)	(N/M ²)	
	Torque	7.7-8.2 N	IM		
	Example 26				
		Film			
15		Blowing		Work	Feed
		Zone	<u>Zone</u>	<u>Zone</u>	Zone
		040			
		213	209	208	194
20	Example 27				
20	DAGMPIE 27	Film			
		Blowing		Work	Feed
		Zone	Zone	<u>Zone</u>	Zone
2-		0.1.0			
25		210	208	202	194
	Example 28				
	Mygmbre 70	Film			
			n .		
2.0		Blowing		Work	Feed
30		Zone	<u>Zone</u>	<u>Zone</u>	<u>Zone</u>

209

210

204

- 20 -

Example 29

Ingredients

5 5 kg PVA
5% w/w stearamide (0.25 kg)
5% w/w glycerol (0.25 kg)

Temperatures

10 Film

Blowing Die Work Feed
Zone Zone Zone Zone

211 211 207 202

Pressure

 $35-40 \text{ bar } (3500-4000 \text{ kN/m}^2)$

Torque

7.9-8.2 NM

RPM

303

The quality of the film produced was good

Example 30

Ingredients

25

15

5 kg PVA

4% w/w stearamide (0.20 kg)

5% w/w glycerol (0.25 kg)

30 <u>Temperatures</u>

Film

Blowing Die Work Feed

Zone Zone Zone Zone

35 212 210 207 202

- 21 -

Pressure

45-50 bar $(4500-5000 \text{ kN/m}^2)$

Torque

8-8.3 NM

RPM

301

5

The quality was poor and the film produced was not commercial quality.

Example 31

10 <u>Ingredients</u>

5 kg PVA

3% w/w stearamide (0.15 kg)

5% w/w glycerol (0.25 kg)

15

Temperatures

Film

212

Blowing Die Work Feed Zone <u>Zone</u> <u>Zone</u> <u>Zone</u>

208

202

20

210

48-50 bar $(4800-5000 \text{ kN/M}^2)$ Pressure

8.3-8.5 NM Torque

25 RPM 303

The film produced was poor quality.

Example 32

30

<u>Ingredients</u>

5 kg PVA

2% w/w stearamide (0.10 kg)

5% w/w glycerol (0.25 kg) 35

- 22 -

Temperatures

Film

Blowing Die Work Feed

Zone Zone Zone Zone

212 212 209 202

Pressure

58-60 bar $(5800-6000 \text{ kN/m}^2)$

10 Torque

9.1-9.4 NM

RPM

5

303

The film produced was poor quality.

15 Example 33

Ingredients

5 kg PVA

20 1% w/w stearamide (0.05 kg)

5% w/w glycerol (0.25 kg)

<u>Temperatures</u>

Film

 25
 Blowing
 Die
 Work
 Feed

 Zone
 Zone
 Zone
 Zone

212 215 210 202

30 Pressure

60-64 bar $(6000-6400 \text{ kN/m}^2)$

Torque

9.7-10.4 NM

RPM

303

The quality produced was poor.

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Example 34

Ingredients

5 5 kg PVA
7.5% w/w stearamide (0.375 kg)

Temperatures

10 Film

 Blowing
 Die
 Work
 Feed

 Zone
 Zone
 Zone

 212
 209
 201
 198

15

Pressure 40 bar (4000 kN/M^2)

Torque 7.1-7.4 NM

Very poor quality film produced.

20

Example 35

Ingredients

25 5 kg PVA

5% w/w stearamide (0.25 kg)
4% w/w glycerol (0.20 kg)

Temperatures

30 Film

 Blowing
 Die
 Work
 Feed

 Zone
 Zone
 Zone
 Zone

 214
 219
 211
 199

- 24 -

Torque

9.5-9.9 NM

The quality of the film produced was good.

5

Example 36

Ingredients

10 5 kg PVA

5% w/w stearamide (0.25 kg)
3% w/w glycerol (0.15 kg)

The quality of the film produced was poor.

15

Example 37

Ingredients

20 5 kg PVA

5% w/w stearamide (0.25 kg) 2% w/w glycerol (0.10 kg)

Very poor quality film produced.

25

The following examples detail the compounding temperatures resulting from processing the material under various different conditions at the pre-mixing stages.

30 Example 38

The PVA/stearamide and glycerol were heated to 140°C in the forced action blender.

- 25 -

Temperatures at compounding stage

Film

 Blowing
 Die
 Work
 Feed

 Zone
 Zone
 Zone
 Zone

 214
 212
 210
 197

Pressure

50-55 bar $(5000-5500 \text{ kN/m}^2)$

10 Torque

8.1-8.6 NM

The quality of the film produced was good.

Example 39

15

5

The mix was heated to 145°C during the pre-mix stage.

Temperatures at compounding stage

Film

 Zone
 Zone
 Zone
 Zone
 Zone
 Zone

 213
 213
 211
 197

25 Pressure

65 bar (6500 kN/m^2)

Torque

8.6-8.9 NM

The quality was borderline acceptable.

30 Example 40

The mix was heated to 150° C during the pre-mix stage.

- 26 -

211

.197

Temperatures at compounding stage

Film

215

Blowing Die Work Feed
Zone Zone Zone

214

5

Pressure 65 bar (4000 kN/m^2)

Torque

8.6-8.9 NM

10

The quality was borderline acceptable.

Example 41

15 The mix was heated to 160° C during the pre-mix stage.

Temperatures at compounding stage

Film

20 Zone Zone Zone Zone Zone 213 209 210 198

Pressure

40 bar (4000 kN/m^2)

25 Torque

7.1-7.3 NM

These parameters produced poor quality film.

Example 42

30 _ _

The mix was heated to 119°C during the pre-mix stage.

- 27 -

Temperatures at compounding stage

Film

 Blowing
 Die
 Work
 Feed

 Zone
 Zone
 Zone
 Zone

 214
 215
 211
 197

Pressure

70 bar (7000 kN/m^2)

Torque

9.0-9.4 NM

10

5

The quality of the film produced was good.

Example 43

15 The mix was heated to 117°C during the pre-mix stage.

Temperatures at compounding stage

Film

20	Blowing	Die	Work	Feed
	Zone	<u>Zone</u>	Zone	Zone
	216	215	211	197

Pressure

 $68-70 \text{ bar } (6800-7000 \text{ kN/m}^2)$

25 Torque

8.7-9.0 NM

The quality of the film produced was good.

Example 44

30

The mix was heated to 113°C during the pre-mix stage.

- 28 -

Temperatures at compounding stage

Film

Blowing	Die	Work	Feed
Zone	Zone	Zone	Zone
213	215	211	196

Pressure $70-75 \text{ bar } (7000-7500 \text{ kN/M}^2)$

Torque

9.2-9.6 NM

10

5

The quality of the film produced was good.

Example 45

15 The mix was heated to 106° C during the pre-mix stage.

Temperatures at compounding stage

Film

Blowing Die Work Feed 20 Zone <u>Zone</u> <u>Zone</u> Zone 214 217 212 196

Pressure

75-80 bar $(7500-8000 \text{ kN/m}^2)$

25 Torque

9.6-10.0 NM

The quality of the film produced was good.

Example 46

30

The mix was heated to 100°C during the pre-mix stage.

- 29 -

Temperatures at compounding stage

Film

Blowing	Die	Work	Feed
Zone	<u>Zone</u>	Zone	<u>Zone</u>
213	213	209	195

Pressure

70-80 bar $(7000-8000 \text{ kN/m}^2)$

Torque

8.1-8.4 NM

10

5

The quality of the film produced was not commercial quality.

The improvements to biodegradable PVA plastics materials described herein can be summarised as follows:-

15

- 1. The PVA can be readily formed and worked to produce a non-laminated layer of PVA as a film or a shaped article.
- Any or each surface of the film or article may be treated to render
 it water resistant.
 - 3. This PVA plastics product, when ruptured and/or immersed in water will dissolve completely and will biodegrade to completion over a period of about 28 days excluding the phenoxy resin waterproofing agent which does not biodegrade.
 - All the components used in the manufacture of the PVA are foodgrade additives.
- 30 It will of course be understood that the invention is not limited to the specific details described herein, which are given by way of example only, and that various modifications and alterations are possible within the scope of the appended claims.

CLAIMS:

- A method of manufacturing a biodegradable plastics material comprising mixing partially hydrolysed, water soluble polyvinyl alcohol
 (PVA) co-polymer with a plasticiser and stabiliser at a temperature in the range of between 106 to 140°C, whereby the resultant material can readily be worked by known processes and is suitable for the manufacture of water soluble and biodegradable articles.
- 10 2. A method according to Claim 1, wherein the method comprises the following steps:
 - a. mixing the stabiliser with the PVA; and
- 15 b. adding the plasticiser to the mixture of stabiliser and PVA and mixing at a temperature between 106 to 140°C.
- A method according to Claim 1 or Claim 2, wherein after mixing the PVA, stabiliser and plasticiser, the method includes the steps of compounding the resultant product to produce a useable, commercial material wherein the compounding is carried out at a temperature in the range 195 225°C.
- 4. A method according to Claim 3, including the step of pelletising the 25 resultant product to produce a useable, commercial pellet.
 - 5. A method according to any preceding claim, wherein the method includes processing the plastics material further by blow moulding, cast extrusion, injection moulding or any other suitable plastics processing procedure.
 - 6. A method according to any preceding claim, including mixing PVA and stabiliser in a forced action blender.
- 35 7. A method according to any preceding claim, characterised in that the

stabiliser is included in an amount in the range of 4 to 6% w/w (weight of stearamide to weight of PVA).

- 8. A method according to any one of Claims 1 to 6, characterised in that the plasticiser is included in an amount in the range of 3 to 15% w/w (weight of plasticiser to weight of PVA).
 - 9. A method according to any preceding claim, wherein the stabiliser is stearamide or a stearate.
 - 10. A method according to any preceding claim, characterised in that the plasticiser comprises glycerol or glycerine solution or soya bean oil.
- 11. A method according to any one of the preceding claims characterised in that the mixing of PVA, stabiliser and plasticiser is carried out at a temperature in the range of 116 to 135°C.
- 12. A method according to any one of the preceding claims characterised in that the mixing of PVA, stabiliser and plasticiser is carried out at a temperature in the range of 123 to 129°C.
 - 13. A method according to any of Claims 5 to 12 including the step of applying a waterproofing agent to at least a portion of the surface of the plastics material so that at least a portion of the material is rendered resistant to water to prevent premature dissolution of the product on contact with water.
 - 14. A method according to Claim 13, wherein the waterproofing agent is phenoxy resin.
 - 15. A biodegradable, plastics material produced by a method as claimed in any preceding claim.
- 16. An article produced by the method as claimed in any one of Claims 1 35 to 15, wherein the article is fully or substantially fully biodegradable.

25

30

17. An article produced by the method as claimed in any one of Claims 1 to 15, wherein the biodegrading of the article commences on contact of the article with water.

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18. A method according to any one of the preceding claims, wherein PVA feedstock may be cold or hot soluble, partially hydrolysed PVA which is 70-85 wt % polyvinyl alcohol.

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A. CLASSIFICATION OF SUBJECT MATTER IPC 6 C08L29/04 C08K5/00

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols) IPC 6 COBK COBL

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

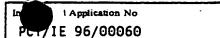
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X Further documents are listed in the continuation of box C.	X Patent family members are listed in annex.
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Date of the actual completion of the international search 6 January 1997	Date of mailing of the international search report 2 2. 01, 97
Name and mailing address of the ISA European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo nl, Fax: (+31-70) 340-3016	Authorized officer Kaumann, E

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INTERNATIONAL SEARCH REPORT



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